

Structural Calculations Cover Sheet

Project Number: 2022.059
Project Name: Wai

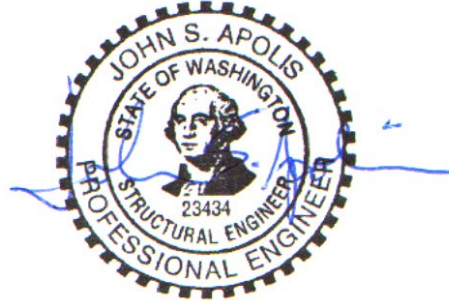
Date: October 2, 2023
Architect: Shawn Sullivan

Structural Design For: Structural design for an addition and remodel

Construction Type: Conventional wood platform framing with conventional concrete foundations

CODES

2018 International Building Code (IBC)
2018 NDS
ASCE 7-16



LOADS

Dead Loads As required
Floor Load 40 psf
Roof Load 25 psf
Wind 110 mph, Exposure C, Per ASCE 7-16 Section 28, $K_{zt} = 1.0$
Seismic Per ASCE 7-16 Section 12
Peak Ground Accelerations (PGA) based on USGS Hazards Program 2003, by Lat/Lon.
PGA 1 sec $\approx .502$ PGA .2 sec = 1.453 %V = .149 * DL

Material Design Values

Soils (assumed) Minimum 1,500 psf allowed bearing (subject to field verification)
Concrete $f'_c=2,500$ psi; 5-1/2 sack mix, or alternate mix pre-approved by bldg. dept.
Reinforcing Grade 60; $F_y=60,000$ psi minimum
Sawn Lumber Joists, Rafters: Hem-Fir #2 and better
Beams, Posts: DF-L #2
Studs & Plates: Hem-Fir Standard
Glu-Lam Beams 24F-V4 for simple span beams, 24F-V8 for cantilevered beams
Parallam Beams 2.2E PSL, $F_b=2,900$ psi, $F_v=290$ psi, $E=2.2 \times 10^6$ psi (minimum)
Microllam Beams 1.9E LVL, $F_b=2,600$ psi, $F_v=285$ psi, $E=1.9 \times 10^6$ psi (minimum)
Timberstrand Bms 1.7E LSL, $F_b=2,600$ psi, $F_v=400$ psi, $E=1.7 \times 10^6$ psi (minimum)
Anchor Bolts F1554 Anchor Bolts, A307 other bolts

John S. Apolis, P.E.

CSES, Inc.

Job number: 2022.059

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Date: 7-Jul-23

Architect:

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BEAM DESIGN (Uniform Load+Concentrated Load)

2018 International Building Code (IBC)

2018 NDS

Beam Description: SOUTH DECK BEAM

Fully Supported:	1	Snow Load:		Wind Load:	
Repetitive Member:		P.T. Lumber:		Wet Use:	

Geometry and Loads:

Span:	18.5 ft	Tributary Width:	3 ft	P Location:	18.5 ft
Add'l uniform DL:		DL unit load:	12 psf	Concentrated DL:	
Add'l uniform LL:		LL unit load:	60 psf	Concentrated LL:	
Add'l uniform SL:		SL unit load:		Concentrated SL:	
Add'l uniform WL:		WL unit load:		Concentrated WL:	

DL Reaction 1:	333 lbs	DL Reaction 2:	333 lbs	Note: Design automatically uses ASD load combinations
LL Reaction 1:	1665 lbs	LL Reaction 2:	1665 lbs	
SL Reaction 1:	0 lbs	SL Reaction 2:	0 lbs	
WL Reaction 1:	0 lbs	WL Reaction 2:	0 lbs	
Total Reaction 1:	1998 lbs	Total Reaction 2:	1998 lbs	

Material Properties:

E	1.8 msi	E'	1.8 msi
Fb	2400 psi	Fb'	2400 psi
Fv	265 psi	Fv'	265 psi
Fc perp	650 psi	Fc perp'	650 psi
Emin	0.95 msi	Emin'	0.95 msi

Deflection analysis:

For total load: Allowed deflection criteria, span/	240		
For LL only: Allowed deflection criteria, span/	360		
Max. allowed total defl:	0.93 in	Max LL defl:	0.62 in
Total defl. * I:	316.26 in^4	Required I:	341.91 in^4
LL defl. * I:	263.55 in^4	Required I:	427.38 in^4
Actual deflections: TOTAL:	0.63 in		0.52 in

Force analysis:

Max. moment:	9241 ft-lb	Max Shear:	1998 lbs
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Selected Member: (1) GLB 3.5 x 12

Member properties:	Provided:	Required:
Moment of inertia:	504. in^4	427.38 in^4
Section Modulus:	84. in^3	46.2 in^3
Section Area:	42. in^2	11.31 in^2
Bearing Area:		3.07 in^2
Minimum bearing dimensions:	3.5 in x	0.88 in

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BEAM DESIGN (Uniform Load+Concentrated Load)

2018 International Building Code (IBC)

2018 NDS

Beam Description: *BEAM SUPPORTING ENTRY*

Fully Supported:	1	Snow Load:	1	Wind Load:	
Repetitive Member:		P.T. Lumber:		Wet Use:	

Geometry and Loads:

Span:	9.5 ft	Tributary Width:	3 ft	P Location:	9.5 ft
Add'l uniform DL:		DL unit load:	25 psf	Concentrated DL:	
Add'l uniform LL:		LL unit load:	60 psf	Concentrated LL:	
Add'l uniform SL:		SL unit load:	25 psf	Concentrated SL:	
Add'l uniform WL:		WL unit load:		Concentrated WL:	

DL Reaction 1:	356 lbs	DL Reaction 2:	356 lbs	Note: Design automatically uses ASD load combinations
LL Reaction 1:	855 lbs	LL Reaction 2:	855 lbs	
SL Reaction 1:	356 lbs	SL Reaction 2:	356 lbs	
WL Reaction 1:	0 lbs	WL Reaction 2:	0 lbs	
Total Reaction 1:	1265 lbs	Total Reaction 2:	1265 lbs	

Material Properties:

E	1.6 msi	E'	1.6 msi
Fb	900 psi	Fb'	1242 psi
Fv	180 psi	Fv'	207 psi
Fc perp	625 psi	Fc perp'	625 psi
Emin	0.58 msi	Emin'	0.58 msi

Deflection analysis:

For total load: Allowed deflection criteria, span/		240	
For LL only: Allowed deflection criteria, span/		360	
Max. allowed total defl:	0.48 in	Max LL defl:	0.32 in
Total defl. * I:	37.8 in^4	Required I:	79.58 in^4
LL defl. * I:	29.21 in^4	Required I:	92.23 in^4
Actual deflections:	TOTAL: 0.16 in		0.13 in

Force analysis:

Max. moment:	3004 ft-lb	Max Shear:	1265 lbs
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Selected Member: (1) DF #2 3.5 x 9.25

(MIN. REQUIRED, UPGRADE MAY BE PROVIDED)

Member properties:	Provided:	Required:
Moment of inertia:	230.84 in^4	92.23 in^4
Section Modulus:	49.91 in^3	29.02 in^3
Section Area:	32.38 in^2	9.16 in^2
Bearing Area:		2.02 in^2
Minimum bearing dimensions:	3.5 in x	0.58 in

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Architect:

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BEAM DESIGN (Uniform Load+Concentrated Load)

2018 International Building Code (IBC)

2018 NDS

Beam Description: *CENTRAL BEAM LINE LONGEST SPAN*

Fully Supported:	1	Snow Load:		Wind Load:	
Repetitive Member:		P.T. Lumber:	1	Wet Use:	

Geometry and Loads:

Span:	9 ft	Tributary Width:	4.5 ft	P Location:	9 ft
Add'l uniform DL:		DL unit load:	12 psf	Concentrated DL:	
Add'l uniform LL:		LL unit load:	60 psf	Concentrated LL:	
Add'l uniform SL:		SL unit load:		Concentrated SL:	
Add'l uniform WL:		WL unit load:		Concentrated WL:	

DL Reaction 1:	243 lbs	DL Reaction 2:	243 lbs	Note: Design automatically uses ASD load combinations
LL Reaction 1:	1215 lbs	LL Reaction 2:	1215 lbs	
SL Reaction 1:	0 lbs	SL Reaction 2:	0 lbs	
WL Reaction 1:	0 lbs	WL Reaction 2:	0 lbs	
Total Reaction 1:	1458 lbs	Total Reaction 2:	1458 lbs	

Material Properties:

E	1.6 msi	E'	1.52 msi
Fb	900 psi	Fb'	864 psi
Fv	180 psi	Fv'	144 psi
Fc perp	625 psi	Fc perp'	625 psi
Emin	0.58 msi	Emin'	0.551 msi

Deflection analysis:

For total load: Allowed deflection criteria, span/		240	
For LL only: Allowed deflection criteria, span/		360	
Max. allowed total defl:	0.45 in	Max LL defl:	0.3 in
Total defl. * I:	31.47 in^4	Required I:	69.93 in^4
LL defl. * I:	26.22 in^4	Required I:	87.41 in^4
Actual deflections:	TOTAL: 0.14 in		0.11 in

Force analysis:

Max. moment:	3281 ft-lb	Max Shear:	1458 lbs
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Selected Member: (1) DF #2 3.5 x 9.25

Member properties:	Provided:	Required:
Moment of inertia:	230.84 in^4	87.41 in^4
Section Modulus:	49.91 in^3	45.56 in^3
Section Area:	32.38 in^2	15.19 in^2
Bearing Area:		2.33 in^2
Minimum bearing dimensions:	3.5 in x	0.67 in

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Architect:

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BEAM DESIGN (Uniform Load+Concentrated Load)

2018 International Building Code (IBC)

2018 NDS

Beam Description: *NEW HEADER*

Fully Supported:	1	Snow Load:		Wind Load:	
Repetitive Member:		P.T. Lumber:		Wet Use:	

Geometry and Loads:

Span:	7.5 ft	Tributary Width:	7 ft	P Location:	7.5 ft
Add'l uniform DL:	30 lbs/ft	DL unit load:	15 psf	Concentrated DL:	
Add'l uniform LL:	150 lbs/ft	LL unit load:	40 psf	Concentrated LL:	
Add'l uniform SL:		SL unit load:		Concentrated SL:	
Add'l uniform WL:		WL unit load:		Concentrated WL:	

DL Reaction 1:	506 lbs	DL Reaction 2:	506 lbs	Note: Design automatically uses ASD load combinations
LL Reaction 1:	1613 lbs	LL Reaction 2:	1613 lbs	
SL Reaction 1:	0 lbs	SL Reaction 2:	0 lbs	
WL Reaction 1:	0 lbs	WL Reaction 2:	0 lbs	
Total Reaction 1:	2119 lbs	Total Reaction 2:	2119 lbs	

Material Properties:

E	1.8 msi	E'	1.8 msi
Fb	2400 psi	Fb'	2400 psi
Fv	265 psi	Fv'	265 psi
Fc perp	650 psi	Fc perp'	650 psi
Emin	0.95 msi	Emin'	0.95 msi

Deflection analysis:

For total load: Allowed deflection criteria, span/		240	
For LL only: Allowed deflection criteria, span/		480	
Max. allowed total defl:	0.38 in	Max LL defl:	0.19 in
Total defl. * I:	22.35 in^4	Required I:	59.59 in^4
LL defl. * I:	17.01 in^4	Required I:	90.7 in^4
Actual deflections:	TOTAL: 0.18 in		0.14 in

Force analysis:

Max. moment:	3973 ft-lb	Max Shear:	2119 lbs
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Selected Member: (1) GLB 3.5 x 7.5

Member properties:	Provided:	Required:
Moment of inertia:	123.05 in^4	90.7 in^4
Section Modulus:	32.81 in^3	19.86 in^3
Section Area:	26.25 in^2	11.99 in^2
Bearing Area:		3.26 in^2
Minimum bearing dimensions:	3.5 in x	0.93 in

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 Project: Wai
 Architect:

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Job number: 2022.059
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BEAM DESIGN (Uniform Load+Concentrated Load)

2018 International Building Code (IBC) 2018 NDS

Beam Description: NEW GARAGE DOOR HEADER

Fully Supported:	1	Snow Load:	1	Wind Load:	
Repetitive Member:		P.T. Lumber:		Wet Use:	

Geometry and Loads:

Span:	19.5 ft	Tributary Width:	2 ft	P Location:	10 ft
Add'l uniform DL:		DL unit load:	30 psf	Concentrated DL:	2340 lbs
Add'l uniform LL:		LL unit load:	40 psf	Concentrated LL:	3120 lbs
Add'l uniform SL:		SL unit load:	25 psf	Concentrated SL:	1950 lbs
Add'l uniform WL:		WL unit load:		Concentrated WL:	

DL Reaction 1:	1785 lbs	DL Reaction 2:	1725 lbs	Note: Design automatically uses ASD load combinations
LL Reaction 1:	2380 lbs	LL Reaction 2:	2300 lbs	
SL Reaction 1:	1488 lbs	SL Reaction 2:	1438 lbs	
WL Reaction 1:	0 lbs	WL Reaction 2:	0 lbs	
Total Reaction 1:	4686 lbs	Total Reaction 2:	4528 lbs	

Material Properties:

E	1.8 msi	E'	1.8 msi
Fb	2400 psi	Fb'	2700 psi
Fv	265 psi	Fv'	305 psi
Fc perp	650 psi	Fc perp'	650 psi
Emin	0.95 msi	Emin'	0.95 msi

Deflection analysis:

For total load: Allowed deflection criteria, span/		240	
For LL only: Allowed deflection criteria, span/		360	
Max. allowed total defl:	0.98 in	Max LL defl:	0.65 in
Total defl. * I:	1441.33 in ⁴	Required I:	1478.28 in ⁴
LL defl. * I:	986.17 in ⁴	Required I:	1517.18 in ⁴
Actual deflections:	TOTAL: 0.93 in		0.64 in

Force analysis:

Max. moment:	37406 ft-lb	Max Shear:	4686 lbs
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Selected Member: (1) GLB 5.5 x 15

Member properties:	Provided:	Required:
Moment of inertia:	1546.88 in ⁴	1517.18 in ⁴
Section Modulus:	206.25 in ³	166.25 in ³
Section Area:	82.5 in ²	23.06 in ²
Bearing Area:		7.21 in ²
Minimum bearing dimensions:	5.5 in x	1.31 in

STEEL ALTERNATIVE: $I_{min} = 96 in^4 < 98 in^4$ W8x28
 $M_{cap} = 44 k-ft > 37 k-ft$ OK

FOOTING DESIGN:

$$\frac{1998 \# \times 2}{1500 \text{ psf}} = 384 \text{ in}^2 < 24 \text{ in} \times 24 \text{ in} = 576 \text{ in}^2 \quad \checkmark \text{OK}$$

$$\text{PIPE PILE CAPACITY} = 3 \times [6000 \# \times 5 / (5^2 + 12)^{1/2}] = 17,651 \#$$

$$1998 \# \times 2 = 3996 \# < 17,651 \# \quad \checkmark \text{OK}$$

USE 24" X 24" X 12" DEEP FOOTINGS W/ (3) #4 EACH WAY, SUPPORTED BY PIPE PILES PER DETAIL PI.

CONSULTING STRUCTURAL ENGINEERING SERVICES

Residential and Commercial Structural Design

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Project No. 2022-059 Date 10/2/23

Project Name CAMPBELL

Comments _____

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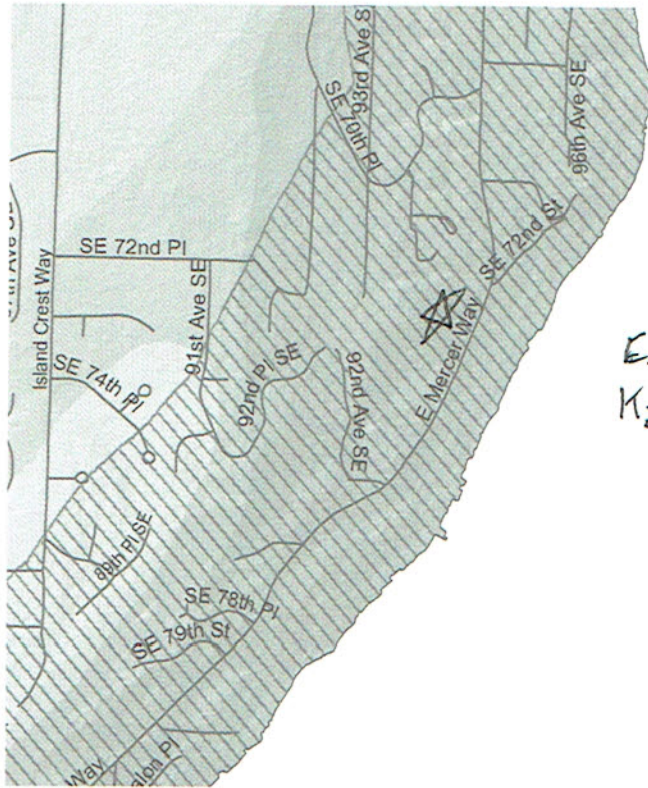
7235 E Mercer Way, Mercer Island, WA 98040, USA

Latitude, Longitude: 47.53745139999999, -122.2131888



Date	5/19/2022, 11:39:20 AM
Design Code Reference Document	ASCE7-16
Risk Category	II
Site Class	D - Default (See Section 11.4.3)

Type	Value	Description
S_S	1.453	MCE_R ground motion. (for 0.2 second period)
S_1	0.502	MCE_R ground motion. (for 1.0s period)
S_{MS}	1.743	Site-modified spectral acceleration value
S_{M1}	null -See Section 11.4.8	Site-modified spectral acceleration value
S_{DS}	1.162	Numeric seismic design value at 0.2 second SA
S_{D1}	null -See Section 11.4.8	Numeric seismic design value at 1.0 second SA



Exp. C
 $K_{zt} = 1.0$

Lateral Loads Design per ASCE 7-16, Wind: Section 28 Seismic: Section 12

(Simplified Envelope Procedure Part 2)

2018 International Building Code (IBC)

WIND LOADS 110 mph Basic Wind Speed 2015 NDS
 $P_s = \lambda * K_{zt} * P_s(30) * 0.6$ Exposure **C** Roof Slope: **4.00** : 12 = 18.4
 Least Horizontal Dimension, feet: **50** Mean Roof Ht, feet: **23** (degrees)
 $\lambda = 1.33$ $a = 5.0$ ft, $2a = 10.0$ ft
 $I_w = 1.00$ $K_{zT} = 1.00$

<u>Tabulated Ps(30):</u> (Refer to ASCE 7-16, Figure 28.6-1)	<u>Zone</u>	<u>Tabulated Wind Pressure</u>	<u>Calc'd Design Pressure</u> (*lambda*KzT*0.6)	<u>Min Design Pressure</u>	(Per section 28.6.4 minimum wind pressure is 16 PSF for zones A,C, and 8 PSF for zones B, D)
(horizontal)	A	25.8	psf 20.5	20.5	
"	B	-7.3	psf -5.8	6.4	
"	C	17.2	psf 13.7	13.7	
"	D	-4.1	psf -3.3	6.4	
(vertical)	E	-23.1	psf -18.4		
"	F	-15.7	psf -12.5		
"	G	-16.0	psf -12.7		
"	H	-12.0	psf -9.5		
(uplift on overhangs)	E(oh)	-32.3	psf -25.7		
"	G(oh)	-25.3	psf -20.1		

(Equivalent Lateral Force Procedure, Section 12.8)

SEISMIC LOADS $I_e = 1.0$ $R = 6.5$ ASCE 7-16, Table 12.2.1
 Seismic Parameters Group I Site Class: **D**
 per ASCE 7-16) $PGA (.2 \text{ sec}) = 1.453$ $F_a = 1.00$ ASCE 7-16 Table 11.4-1
 $PGA (1 \text{ sec}) = 0.502$ $F_v = 1.50$ ASCE 7-16 Table 11.4-2

Seismic Design Categories per ASCE 7-16 Tables 11.6-1, 11.6-2

Based on S_d s: **D** Based on S_{d1} : **D**

PGA's based on peak ground accelerations per latest USGS Hazards Program (based on lat/lon).

$S_s = 1.4530$ $S_{ms} = F_a * S_s = 1.45$ Equation 11.4-1
 $S_1 = 0.5020$ $S_{m1} = F_v * S_1 = 0.75$ Equation 11.4-2

Equations 11.4-3, 11.4-4 $S_d = 2/3 * S_{ms} = 0.97$ $S_{d1} = 2/3 * S_{m1} = 0.50$
 Equation 12.14-11 $C_s \text{ (or \%V)} = (S_d / (R/I)) = 0.149$ **Building period < 0.5 s per IBC eq 12.8-7**

Base Shear = %V * W * 0.7 = 4.38 psf, uniformly distributed over floor area
 (0.7 reduction factor per ASCE 7-16, Section 2.4.1, Eq 5 (seismic vertical distribution per IBC eqs 12.8-11 & 12)

	<u>Roof or Floor DL (psf)</u>	<u>Wall DL (psf)</u>	<u>Story Height Above Base (ft)</u>	<u>Lateral Load (psf)</u>
Base = top of foundation	DL (psf)	dist. over floor area	Above Base (ft)	
Top Framing	12	6	17	2.57
Main Floor	12	12	9	1.81
				0.00
Total Seismic DL:	42		Sum	4.38

SHEAR WALL DESIGN - EAST WALL - LOWER FLOOR - L = 5' + 21.5'

$$P_w = 10' \times 15.5' \times 20.5 \text{ psf} + 8' \times 16.5' \times 13.7 \text{ psf} = \underline{4,986^\#}$$

$$P_e = 10' \times 50' \times (2.57 + 1.81) \text{ psf} = 3,942^\#$$

$$V = \frac{4,986^\#}{230 \text{ pif}} = 21.6' \text{ MIN.} \quad 26.5' \text{ PROVIDED} \quad \underline{\text{SWI OK}}$$

$$\text{UPLIFT} = 8' \times \frac{4,986^\#}{26.5'} = 1,505^\# < 4,065^\# \quad \underline{\text{HOU5}}$$

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